

Author: G. Morgan and R. Fernow  
 Date: June 18, 1984  
 No.: 77-1  
 Title: Expected Short Sample Performances of SSC-P-11  
 Task Force: Coil Geometry Analysis

M. Anerella  
 F. Atkinson  
 G. Bagley  
 A. Bertsche  
 E. Bleser  
 D. Brown  
 V. Buchanan  
 J. Cottingham  
 J. Cullen  
 P. Dahl  
 Y. Elisman  
 A. Feltman  
 R. Fernow  
 G. Ganetis  
 D. Gardner  
 A. Ghosh  
 C. Goodzeit  
~~M. Garber~~  
 A. Greene  
 H. Hahn  
 W. Harrison  
 J. Herrera  
 R. Gupta

R. Hogue  
 S. Kahn  
 E. Kelly  
 H. Kirk  
 J. Koehler  
 R. Louttit  
 R. LeRoy  
 W. McGahern  
 G. Morgan  
 R. Palmer  
 S. Plate  
 I. Polk  
 A. Prodell  
 K. Robins  
 R. Rosenka  
 W. Sampson  
 W. Schneider  
 M. Shapiro  
 R. Shutt  
 J. Skaritka  
 A. Stevens  
 C. Sylvester

P. Thompson  
 P. Wanderer  
 T. Wild  
 E. Willen  
 R. Rau

Expected Short Sample Performances of SSC-P11

G. Morgan and R. Fernow

The central and peak fields of coil design P11, which consists of 2 layers of standard CBA cable run with out current 1.35 times inner, are given in Table 1 at two inner currents as computed using program MDP with iron model DBL15B.

Table 1.

I <sub>in</sub>	B <sub>o</sub>	B <sub>pk,in</sub>	B <sub>pk,out</sub>	I <sub>c,in</sub>	I <sub>c,out</sub>
3500	50983	54505	43974	4472	5731
4500	63954	68362	54981	2997	4401

The peak field points are located about 15% of the distance from the upper inner corner to the upper outer corner of the turn nearest the pole. The critical currents are based on measured values as follows:

5T, 5584A, 5.5T, 4972 A (4.22 K, field perpendicular).

The critical currents of Table 1 assume boiling helium at 19 psia, 4.504K. The correlation used is:

$$I_c = P_1 \left( 1 - \frac{T-4.2}{P_2+P_3B} \right) \left( \frac{1 + P_4B}{1 + P_5B+P_6B^2} \right) \quad (1)$$

where  $P_2 = 4.996$ ,  $P_3 = -0.465$ ,  $P_4 = -.10263$ ,  $P_5 = .31525$  and  $P_6 = -.030335$ , T is temperature (K) and B is field in tesla; this correlation is based on data from several sources.  $P_1$  from the two measured critical currents is 21008 and 20905, the average 20957 was used for the  $I_c$  of Table 1. For interpolation in Table 1 the load line (transfer function) is assumed to vary linearly with B.

This gives for an interpolation expression

$$B = T_f I / (1 + aI) \quad (2)$$

The values of  $a$  and  $T_f$  fitting the 3 field points of Table 1 are given in Table 2.

Table 2.

	Bo	Bpk,in	Bpk,out
T	15.961	17.074	10.330
a	2.735-5	2.753-5	2.327-5

By iterative interpolation, the field values given in Table 3 are obtained

Table 3.

Iin	Iout	Bo	Bpk,in	Bpk,out	I <sub>c</sub> in	I <sub>c</sub> ,out
3860	5211	55726	59573	48008	3903	5215

Thus the inner layer has 1% more margin than the outer.

GM:vm