

Accelerator Department
 BROOKHAVEN NATIONAL LABORATORY
 Associated Universities, Inc.
 Upton, NY 11972

ISABELLE Project

Technical Note No. 337

Interim Cable Dipole Coil Design

H. Hahn and R.C. Fernow

December 15, 1981

The dipole coil cross section has been redesigned to take into account the smaller average thickness per turn, $\langle t \rangle$, for the cable currently being supplied by New England Electric. The value of $\langle t \rangle$ at 10 000 psi compression is now 55.0 mils as compared to the 57.4 mils in the original surplus Fermi-lab cable. This has required a readjustment of the original cable magnet design.¹ However, in order to make use of existing material, the centerpost design remains unchanged. It should be satisfactory to use this design until all the manufacturing systematics are understood, at which point a final design iteration may be necessary.

The interim design is given in Table I and Figure 1. Four additional turns have been added giving a total of 105 per quadrant and yielding a transfer function, warm with infinite permeability yoke, of

$\text{wedges} = 4.62^\circ$
 $= 5.65^\circ$

$B/I = 15.64 \text{ G/A.}$

Table I. Dipole Magnet Coil Blocks ($\langle t \rangle = 55 \text{ mils}$, $r_{Fe} = 8.655 \text{ cm}$)

Layer	Block	Turns	ϕ_{start}	ϕ_{end}	$\Delta\phi$	$r_i \text{ (cm)}$	\bar{r}	$r_o \text{ (cm)}$
Inner	2	62	0.04 ^o	71.37 ^o	71.33	6.566	6.957	7.348
Inner	1	4	75.99	80.59	4.60	6.566		7.348
Outer	2	28	0.04	28.81	28.77	7.399	7.790	8.181
Outer	1	11	34.46	45.76	11.30	7.399		8.181

The multipoles generated by this configuration are given in Table II. The primed multipoles are defined as

$$b'_n = b_n (4.4 \text{ cm})^n$$

and are dimensionless quantities. All the multipoles are well within the allowed systematic tolerances except b_6 , which is approximately one tolerance. The overall field is nonetheless quite good with

$$\frac{\Delta B}{B} < 0.3 \times 10^{-4}$$

and

$$\left[\sum_6^\infty (b'_n r^n)^2 \right]^{1/2} \leq 0.9 \times 10^{-4}$$

over the 4.4 cm warm bore aperture, assuming b_2 and b_4 trim coils.

1. R.B. Palmer, Report TLM-22 (1981).

inner: 1.15053° / turn

outer: 1.02750° / turn

Table II. Design Multipoles ($\langle t \rangle = 55$ mils)

n	$b_n [10^{(n+4)} \text{ cm}^n]$	Tolerance	$b'_n \times 10^4$	Tol
2	-89	0.35 ^a	-17.0	
4	175	4.3 ^a	6.4	
6	64	64	0.4	.46
8	-375	1010	-0.5	1.4
10	1190×10^{-14}	16800	0.3	4.6
12	-10500×10^{-16}	285000	-0.5	15

^atrim coil available.

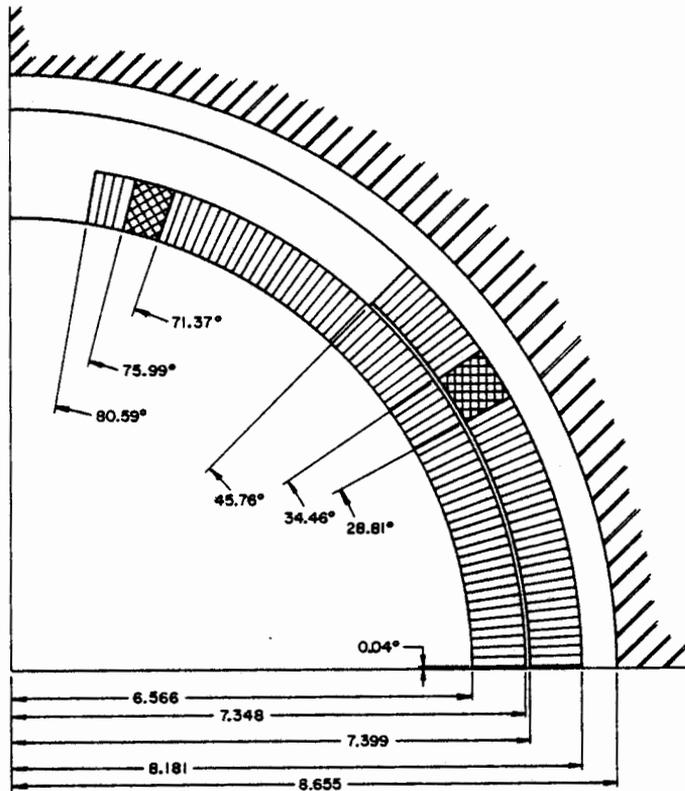


Fig. 1. Coil cross section

Bldg. 911

AD Library
J. Grisoli
D. Lazarus
Y. Lee
D. Lowenstein
M. Smith (1) plus
one for each author(s) file
J.R. Sanford
D.H. White

Bldg. 902

M.Q. Barton
H. Foelsche
H. Hahn
H.J. Halama
R.I. Louttit
R.B. Palmer
E.P. Rohrer
J. Spiro

Bldg. 725

L. Blumberg for
NSLS Library

W.R. Casey, 535A
D.G. Dimmler, 535

Bldg. 510

N. Samios
R.P. Shutt
H. Gordon
T.F. Kycia
L. Leipuner
S. Lindenbaum
S. Ozaki
S. Protopopescu
M. Sakitt
I. Stumer
T.L. Trueman

Magnet Division S&P - 47